June 25, 2012

LMP91200

Configurable AFE for Low-Power Chemical Sensing Applications

General Description

The LMP91200 is a configurable sensor AFE for use in low power analytical sensing applications. The LMP91200 is designed for 2-electrode sensors. This device provides all of the functionality needed to detect changes based on a delta voltage at the sensor. Optimized for low-power applications, the LMP91200 works over a voltage range of 1.8V to 5.5V. With its extremely low input bias current it is optimized for use with pH sensors. Also in absence of supply voltage the very low input bias current reduces degradation of the pH probe when connected to the LMP91200. The Common Mode Output pin (VOCM) provides a common mode offset, which can be programmed to different values to accommodate pH sensor output ranges. For applications requiring a high impedance common mode this option is also available. Two guard pins provide support for high parasitic impedance wiring. Support for an external Pt1000, Pt100, or similar temperature sensor is integrated in the LMP91200. The control of this feature is available through the SPI interface. Additionally, a user controlled sensor diagnostic test is available. This function tests the sensor for proper connection and functionality. Depending on the configuration, total current consumption for the device is 50µA while measuring pH. Available in a 16-pin TSSOP package, the LMP91200 operates from -40°C to +125°C.

Key Specifications

Unless otherwise noted, typical values at

- $T_A = 25^{\circ}$ C, V_S=(VDD-GND) = 3.3V.
- \blacksquare pH Buffer Input bias current (0<V_{INP} <3.3V)
- max @ 25°C ±125 fA $-$ max @ 85 $^{\circ}$ C pH Buffer Input bias current (-500mV<V_{INP}-V_{CM} <500mV), $V_S = (VDD-GND) = 0V$ \equiv max @ 25°C \pm 600 fA — max @ 85°C
oH Buffer Input offset voltage ±200 µV \blacksquare pH Buffer Input offset voltage
- \blacksquare pH Buffer Input offset voltage drift $\pm 2.5 \mu V$ °C ■ Supply current (pH mode) 50 µA
■ Supply voltage 1.8 V to 5.5 V
- Supply voltage 1.8 V to 5.5 V
■ Operating temperature range 40°C to 125°C
- Operating temperature range
- Package 16-Pin TSSOP

Features

- Programmable output current in temperature measurement
- Programmable Output common mode voltage
- Active guarding
- On board sensor test
- Supported by Webench Sensor AFE Designer
- Supported by Webench Sensor Designer Tools

Applications

■ pH sensor platforms

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Ordering Information

Connection Diagram

Pin Descriptions

Absolute Maximum Ratings (*[Note 1](#page-5-0)*)

If Military/Aerospace specified devices are required, please contact the Texas Instruments Sales Office/ Distributors for availability and specifications.

Storage Temperature Range -65° C to 150°C Junction Temperature (*[Note 3](#page-5-0)*) +150°C For soldering specifications: see product folder at www.ti.com and www.ti.com/lit/an/snoa549c/snoa549c.pdf

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Operating Ratings (*[Note 1](#page-5-0)*)

Supply Voltage $(V_s=VDD\text{-GND})$ 1.8V to 5.5V Temperature Range -40° C to 125°C Package Thermal Resistance (θ_{JA}(*[Note 3](#page-5-0)*)) 16-Pin TSSOP 31°C/W

Electrical Characteristics (*[Note 4](#page-5-0)*)

Unless otherwise specified, all limits guaranteed for T_A = 25°C. V_S=(VDD-GND)=3.3V. VREF=3.3V. Boldface limits apply at the temperature extremes.

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Electrical Characteristics (Serial Interface) (*[Note 4](#page-5-0)*)

Unless otherwise specified. All limits guaranteed for $T_A=25^{\circ}$ C, $V_S=(VDD\text{-}GND)=3.3V$.

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Electrical Characteristics (Diagnostic) (*Note 4*)

Unless otherwise specified. All limits guaranteed for $T_A=25^{\circ}$ C, V_S=(VDD-GND)=3.3V.

Note 1: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not guaranteed. For guaranteed specifications and the test conditions, see the Electrical Characteristics **Tables**

Note 2: Human Body Model, applicable std. MIL-STD-883, Method 3015.7. Machine Model, applicable std. JESD22-A115-A (ESD MM std. of JEDEC) Field-Induced Charge-Device Model, applicable std. JESD22-C101-C (ESD FICDM std. of JEDEC).

Note 3: The maximum power dissipation is a function of T_{J(MAX)}, θ_{JA}. The maximum allowable power dissipation at any ambient temperature is

 $P_D = (T_{J(MAX)} - T_A)/\theta_{JA}$. All numbers apply for packages soldered directly onto a PC Board.

Note 4: Electrical Table values apply only for factory testing conditions at the temperature indicated. Factory testing conditions result in very limited self-heating of the device such that TJ = TA. No guarantee of parametric performance is indicated in the electrical tables under conditions of internal self-heating where TJ >TA.

Note 5: Typical values represent the most likely parametric norm as determined at the time of characterization. Actual typical values may vary over time and will also depend on the application and configuration. The typical values are not tested and are not guaranteed on shipped production material.

Note 6: Limits are 100% production tested at 25°C. Limits over the operating temperature range are guaranteed through correlations using the Statistical Quality Control (SQC) method.

Note 7: Boldface limits are production tested at 125°C. Limits are guaranteed through correlations using the Statistical Quality Control (SQC) method.

Note 8: Offset voltage average drift is determined by dividing the change in V_{OS} at the temperature extremes by the total temperature change.

Note 9: Offset voltage long term drift is determined by dividing the change in V_{OS} at time extremes of OPL procedure by the length of the OPL procedure. OPL procedure: 500 hours at 150°C are equivalent to about 15 years.

Note 10: VCMHI voltage average drift is determined by dividing the change in VCMHI at the temperature extremes by the total temperature change.

Note 11: VCMHI_acc vs. VREF is determined by dividing the change in VCMHI_acc at the VREF extremes by the total VREF change.

Note 12: Current source drift is determined by dividing the change in I_{CS} at the temperature extremes by the total temperature change.

- **Note 14:** This parameter is guaranteed by design and/or characterization and is not tested in production.
- **Note 15:** Load for these tests is shown in the timing diagram test circuit.
- **Note 16:** Excluding all currents which flows out from the device.
- **Note 17:** The short circuit test is a momentary open loop test.
- **Note 18:** The voltage on any pin should not exceed 6V relative to any other pins.

Note 19: Short circuit test is a momentary test.

Test Circuit Diagrams

FIGURE 2. SERIAL INTERFACE TIMING DIAGRAM

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FIGURE 3. DIAGNOSTIC TIMING DIAGRAM

Typical Performance Characteristics Unless otherwise specified, T_A=25°C, V_S=(VDD-GND)=3.3V, $V\overline{R}$ FF=3.3V.

pH Buffer Input Bias Current vs. V_{IND} - Device ON

pH Buffer Input Bias Current vs. V_{INP} - Device ON

pH Buffer Input Bias Current vs. VINP - Device ON

pH Buffer Input Bias Current vs. V_{IND} - Device OFF

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pH Buffer Input Bias Current vs. V_{INP} - Device OFF

30165514

pH Buffer Time domain Voltage Noise

30165517

CMRR (dB)

PERCENTAGE (%)

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PGA Gain error vs. Temp

INTEGRATED NOISE (500nV/DIV)

INTEGRATED NOISE (500nV/DIV)

0

0

5

10

15

PERCENTAGE (%)

PERCENTAGE (%)

20

25

30

5

10

15

PERCENTAGE (%)

PERCENTAGE (%)

20

25

UNITS TESTED >5000

30165557

Supply current vs. digital input voltage

30165562

Supply current (Temp Mode) vs. Temperature 450 430 SUPPLY CURRENT (µA) SUPPLY CURRENT (μA) 410 390 Temp Mode, IOUTCS=100uA Temp Mode, IOUTCS=200uA Temp Mode, IOUTCS=1mA Temp Mode, IOUTCS=2mA 370 350 330 310 $290 - 50$ -50 -25 0 25 50 75 100 125 TEMPERATURE (°C)

30165538

Supply current (Temp Mode) vs. Supply Voltage

Functional Description

GENERAL INFORMATION

The LMP91200 is a configurable sensor AFE for use in low power analytical sensing applications. The LMP91200 is designed for 2-electrode sensors. This device provides all of the functionality needed to detect changes based on a delta voltage at the sensor. Optimized for low-power applications, the LMP91200 works over a voltage range of 1.8V to 5.5V. With its extremely low input bias current it is optimized for use with pH sensors. Also in absence of supply voltage the very low input bias current reduces degradation of the pH probe when connected to the LMP91200. The Common Mode Output pin (VOCM) provides a common mode offset, which can be programmed to different values to accommodate pH sensor output ranges. For applications requiring a high impedance common mode this option is also available. Two guard pins provide support for high parasitic impedance wiring. Support for an external Pt1000, Pt100, or similar temperature sensor is integrated in the LMP91200. The control of this feature is available through the SPI interface. Additionally, a user controlled sensor diagnostic test is available. This function tests the sensor for proper connection and functionality.

pH Buffer

The pH Buffer is a unity gain buffer with a input bias current in the range of tens fA at room. Its very low bias current introduces a negligible error in the measurement of the pH. The ph buffer is provided with 2 guard pins (GUARD1, GUARD2) in order to minimize the leakage of the input current and to make easy the design of a guard ring.

Common mode selector and VCM buffer

The common mode selector allows to set 7 different values of common mode voltage (from 1/8 VREF to 7/8VREF with 1/8 VREF step) according to the applied voltage reference at VREF pin. Both buffered and unbuffered version of the set common mode voltage are available respectively at VCM pin and VCMHI pin. A copy of the buffered version is present at VOCM pin in case of differential measurement.

Current Source and PGA

The internal current source is programmable current generator which is able to source 4 different current values (100µA, 200µA, 1mA, 2mA) in order to well stimulate Pt100 and Pt1000 thermal resistor. The selected current is sourced from either RTD pin (pin for thermal resistor connection) or CAL pin (pin for reference resistor connection). The voltage across either the thermal resistor or the reference resistor is amplified by the PGA (5V/V, 10V/V) and provided at the VOUT pin when the LMP91200 is set in Temperature measurement mode.

Output Muxes

The output of the LMP91200 can be configured to support both differential and single ended ADC's. When measuring

pH the Output signal can be referred either to VCM or GND. When measuring temperature the Output signal is referred to GND. The Output configuration is controlled through the SPI interface.

SERIAL CONTROL INTERFACE OPERATION

All the features of the LMP91200 (Mode of Operation, PGA Gain, Voltage reference, Diagnostic) are by data stored in a programming register. Data to be written into the control register is first loaded into the LMP91200 via the serial interface. The serial interface employs a 16-bit shift register. Data is loaded through the serial data input, SDI. Data passing through the shift register is output through the serial data output, SDO_DIAG. The serial clock, SCK controls the serial loading process. All sixteen data bits are required to correctly program the LMP91200. The falling edge of CSB enables the shift register to receive data. The SCK signal must be high during the falling and rising edge of CSB. Each data bit is clocked into the shift register on the rising edge of SCLK. Data is transferred from the shift register to the holding register on the rising edge of CSB.

Configuration Register

Application Information

Theory of pH measurement

pH electrode measurements are made by comparing the readings in a sample with the readings in standards whose pH has been defined (buffers). When a pH sensing electrode comes in contact with a sample, a potential develops across the sensing membrane surface and that membrane potential varies with pH. A reference electrode provides a second, unvarying potential to quantitatively compare the changes of the sensing membrane potential. Nowadays pH electrodes are composed of a sensing electrode with the reference electrode built into the same electrode body, they are called combination electrodes. A high input impedance meter serves as the readout device and calculates the difference between the reference electrode and sensing electrode potentials in millivolts. The millivolts are then converted to pH units according to the Nernst equation.

Electrode behavior is described by the Nernst equation:

$E = E_0 + (2.3 \text{ RT/nF}) \log \text{aH} +$, where

E is the measured potential from the sensing electrode,

Eo is related to the potential of the reference electrode,

(2.3 RT/nF) is the Nernst factor,

 $log aH+$ is the pH, $(aH+ = activity of Hydrogen ions)$.

2.3 RT/nF, includes the Gas Law constant (R), Faraday's constant (F), the temperature in degrees Kelvin (T) and the stoichiometric number of ions involved in the process (n). For pH , where $n = 1$, the Nernst factor is 2.3 RT/F. Since R and F are constants, the factor and therefore electrode behavior is dependent on temperature. The Nernst Factor is equivalent to the electrode slope which is a measure of the electrode response to the ion being detected. When the temperature is 25 °C, the theoretical Nernst slope is 59.16 mV/pH unit.

LMP91200 in pH meter with ATC (Automatic Temperature Compensation)

The most common cause of error in pH measurements is temperature. Temperature variations can influence pH for the following reasons:

the electrode slope will change with variations in temperature; buffer and sample pH values will change with temperature.

Measurement drift can occur when the internal elements of the pH and reference electrodes are reaching thermal equilibrium after a temperature change. When the pH electrode and temperature probe are placed into a sample that varies significantly in temperature, the measurements can drift because the temperature response of the pH electrode and temperature probe may not be similar and the sample may not have a uniform temperature, so the pH electrode and temperature probe are responding to different environments.

The pH values of buffers and samples will change with variations in temperature because of their temperature dependent chemical equilibria. The pH electrode should be calibrated with buffers that have known pH values at different temperatures. Since pH meters are unable to correct sample pH values to a reference temperature, due to the unique pH versus temperature relationship of each sample, the calibration and measurements should be performed at the same temperature and sample pH values should be recorded with the sample temperature.

The LMP91200 offers in one package all the features to build a pH meter with ATC. Through the SPI Interface is possible to switch from pH measurement mode to temperature measurement mode and collect both temperature and potential of sensing electrode.

pH measurement

The output of a pH electrode ranges from 415 mV to −415 mV as the pH changes from 0 to 14 at 25°C. The output impedance of a pH electrode is extremely high, ranging from 10 MΩ to 1000 MΩ. The low input bias current of the LMP91200 allows the voltage error produced by the input bias current and electrode resistance to be minimal. For example, the output impedance of the pH electrode used is 10 M Ω , if an op amp with 3 nA of Ibias is used, the error caused due to this amplifier's input bias current and the source resistance of the pH electrode is 30 mV! This error can be greatly reduced to 1.25µV by using the LMP91200.

The pH measurement with the LMP91200 is straightforward, the pH electrode needs to be connected between VCM pin and INP pin. The voltage at VCM pin represent the internal zero of the system, so the potential of the electrode (voltage at INP pin) will be refered to VCM voltage. The common mode voltage can be set to well fit the input dynamic range of an external ADC connected between VOUT and VOCM when the LMP91200 is configured with differential output. In *Table 1* a typical configuration of the register of the LMP91200 with VCM set at 1/2 of VREF and differential output.

TABLE 1.

Configuration register: pH measurement

Temperature measurement

The LMP91200 supports temperature measurement with RTD like Pt100 and Pt1000. According to the RTD connected to the LMP91200 the right amount of exciting current can be programmed: 100µA for Pt1000 and 1mA for Pt100, resulting in a nominal voltage drop of 100mV for both RTD's at 0°C. This voltage can be amplified, using an internal amplifier with a factor of 5 or 10 V/V. In case of high precision temperature measurement it is possible to connect an external high accuracy resistor and implement a calibration procedure. The exciting current sourced by the LMP91200 can be multiplexed either into the RTD or into the external precision resistor in order to implement a 2-step or 3-step temperature measurement. The multi step temperature measurements allows to remove uncertainty of the temperature signal path.

1-step measurement

In the one step measurement the voltage across the RTD (Pt100, Pt1000) due to the exciting current is amplified and measured. The temperature can be calculated according to the following equation:

$$
Temp(^{\circ}C) = (Pt_{RES_calculated} - Pt_{RES_nominal})/ \text{alpha}
$$

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alpha is the thermal coefficient of the RTD (it depends on the selected Ptres);

Pt_{RES} nominal is the value of the Ptres at 0degC.

Pt_{RES}_calculated = (VOUT_Pt_{RES}/I_Pt)/PGA_GAIN (2) where

VOUT_Pt_{RES} is the amplified voltage across the RTD at VOUT pin (ground referred) when the LMP91200 is configured according to *Table 2*.

I_Pt is the value of the selected exciting current according to the RTD;

PGA_GAIN is the selected gain of the PGA.

Inserting *Equation 2* in *[Equation 1](#page-18-0)* the temperature is given by the following equation:

$$
Temp(^{\circ}C) = Temp(^{\circ}C) = ((VOUT_Pt_{RES}/I_Pt)/PGA_GAIN - Pt_{RES_nominal})/alpha
$$
 (3)

TABLE 2.

Configuration register: 1-step measurement

The 1-step temperature measurement has a precision of about ±3°C.

2-step measurement

This method requires 2 acquisitions and a precision resistor (R_{REF}) connected between CAL and GND pin, (the RTD is always connected between RTD and GND pin). The first acquisitions measure the voltage across the precision resistor in the same condition (source current and PGA gain) of the next temperature measurement in order to remove the uncertainty on the current source value. The second acquisition measures the voltage across the RTD (similar to the 1-step measure), in this case the formula to calculate the temperature is a little bit more complicate in order to take in account the non-ideality of the system (source current error).

Temp(°C) = (PtRES_calculated – PtRES_nominal) / alpha (4)

where

alpha is the thermal coefficient of the RTD (it depends on the selected Ptres);

Ptres_nominal is the value of the Ptres at 0degC.

$$
\text{Pt}_{\text{RES}-}\text{calculated} = (\text{VOUT}_\text{RES}/\text{PGA}_\text{GAN}) / \text{true} \qquad (5)
$$
\n
$$
\text{where}
$$

VOUT_Pt_{RES} is the amplified voltage across the RTD at VOUT pin (ground referred), when the LMP91200 is configured according to *Table 4*.

I_true is the real current which alternatively flows in the external precison resistance R_{BEF} and in the RTD.

PGA_GAIN is the selected gain of the PGA.

I_true=(VOUT_R_{REF})/(PGA_GAIN*R_{REF}) (6)

where

VOUT_R_{RFF} is the amplified voltage across the R_{RFF} at VOUT pin (ground referred), when the LMP91200 is configured according to *Table 3*.

Inserting *Equation 5* and *Equation 6* in *Equation 4* the temperature is given by the following equation:

Temp(°C) = ((VOUT_PtRES /VOUT_RREF)*RREF– PtRES_nominal) /alpha (7)

Bit	Name	Description
D ₁₅	MEAS_MODE	Temp measurement 1
D ₁₄	I MUX	RCAL 1
[D13:D12] I_VALUE		100µA (Pt1000) 00 1 mA (Pt100) 10
D ₁₁	PGA	10 V/V 1
[D10:DB]	VCM	Leave these bits as they have been configured for the pH measurement.
D7	VOCM	GND
D ₆	DIAG_EN	DIAGNOSTIC disabled 0
[D5:DD]	RESERVED	RESERVED

TABLE 4.

Configuration register: 2-step measurement

The 2-step temperature measurement has a precision of about $\pm 0.3^{\circ}$ C (with R_{RFF} @ 0.01% of tolerance) which is good enough in most of pH meter applications.

3-step measurement

This method requires 3 acquisitions and a precision resistor (R_{REF}) connected between CAL and GND pin, (the RTD is always connected between RTD and GND pin). The first two acquisitions measure the voltage across the precision resistor in 2 different conditions (2 different exciting current and 2 PGA gains) in order to remove the uncertainty of the current source value and the offset of the path. The third acquisition measures the voltage across the RTD (similar to the 1-step measure), in this case the formula to calculate the temperature is more complicate in order to take in account the non-ideality of the system (offset, source current error).

Temp(°C) = (PtRES_calculated – PtRES_nominal) / alpha (8)

where

alpha is the thermal coefficient of the RTD (it depends on the selected Ptres);

Ptres nominal is the value of the Ptres at 0degC.

$$
\mathsf{Pt}_{\mathsf{RES_calculated=((VOUT_Pt_{\mathsf{RES}'\mathsf{PGA_GAIN})\text{-}Vos)}} / \newline \hspace*{1.5cm} 1_true \hspace*{1.5cm} (9)
$$

where

VOUT_Pt_{RES} is the amplified voltage across the RTD at VOUT pin (ground referred), when the LMP91200 is configured according to *Table 7*.

I_true is the real current which alternatively flows in the external precison resistance R_{per} and in the RTD.

PGA_GAIN is the selected gain of the PGA.

Vos is the offset of the path.

$$
Vos=(VOUT_R_{REF0}-VOUT_R_{REF1})/5
$$
 (10)

where

VOUT_RREFO is the amplified voltage across the R_{REF} at VOUT pin (ground referred), when the LMP91200 is configured according to *Table 5*.

VOUT_RREF 1^{is} the amplified voltage across the R_{REF} at VOUT pin (ground referred), when the LMP91200 is configured according to *Table 6*.

I_true=(2*VOUT_RREF1-VOUT_RREF0)/(10*RREF) (11)

Inserting *Equation 9*, *Equation 10* and *Equation 11* in *Equation 8* the temperature is given by the following equation:

Temp(°C) = (((VOUT_PtRES/PGA_GAIN)- (VOUT_RREF0-VOUT_RREF1)/5)/((2*VOUT_RREF1- VOUT_RREF0)/(10*RREF))– PtRES_nominal) /alpha (12)

TABLE 5.

Configuration register: 3-step measurement

The 3-step temperature measurement can reach a precision as high as $\pm 0.1^{\circ}$ C (with R_{RFF} @ 0.01% of tolerance) when the analog signal is acquired by at least 16 bit ADC. With lower number of bit ADC this method gives the same result of the 2-step measurement due to the low voltage offset of the signal path. As rule of thumb, the 3-step temperature measurement gives good result if he the LSB of the ADC is less than the input offset of the PGA.

Diagnostic Feature

The diagnostic function allows detecting the presence of the sensor and checking the connection of the sensor. A further analysis of the answer of the pH probe to the diagnostic stimulus allows estimating the aging of the pH probe. With the diagnostic function is possible to change slightly (+/- 5% VREF) the Common mode voltage. If the sensor is present it reacts, this reaction gives some information on the status of the connection, the presence of the sensor and its aging. In fact a typical symptom of the aging of a pH probe is the slowness in the answer. It means that a pH probe answers with a smoother step to the diagnostic stimulus as its age increases.

The procedure is enabled and disabled by SPI (refer to *[Con](#page-17-0)[figuration Register](#page-17-0)*). Until bit D6 is at low logic level, VCM stays at the programmed voltage independently by the SDO_DIAG pin status. When bit D6 is tied at high logic level, on the first rising edge of SDO_DIAG, a positive pulse is generate. At the second positive rising edge of SDO_DIAG pin, the positive pulse ends. At the third positive rising edge of SDO_DIAG a negative pulse is generated. At the forth positive rising edge of the SDO_DIAG the negative pulse ends and the routine is stopped and cannot restart until bit D6 is set again at 1.

Layout Consideration

In pH measurement, due to the high impedance of the ph Electrode, careful circuit layout and assembly are required. Guarding techniques are highly recommended to reduce parasitic leakage current by isolating the LMP91200's input from large voltage gradients across the PC board. A guard is a low impedance conductor that surrounds an input line and its potential is raised to the input line's voltage. The input pin should be fully guarded as shown in *[Figure 4](#page-21-0)*.The guard traces should completely encircle the input connections. In addition, they should be located on both sides of the PCB and be con-

nected together. The LMP91200 makes the guard ring easy to be implemented without any other external op amp. The ring needs to be connected to the guard pins (GUARD1 and GUARD2) which are at the same potential of the INP pin. Solder mask should not cover the input and the guard area including guard traces on either side of the PCB. Sockets are not recommended as they can be a significant leakage source. After assembly, a thorough cleaning using commercial solvent is necessary.

In *Figure 4* is showed a typical guard ring circuit when the LMP912000 is interfaced to a pH probe trough a triaxial cable/ connector, usually known as 'TRIAX'. The signal conductor and the guard of the triax should be kept at the same potential; therefore, the leakage current between them is practically zero. Since triax has an extra layer of insulation and a second conducting sheath, it offers greater rejection of interference than coaxial cable/connector.

FIGURE 4. Circuit Board Guard Layout

Notes

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